

A New 2 K Superconducting Half-Wave Cavity Cryomodule for PIP-II

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On Behalf of the ANL Physics Division Linac Development Group

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 - Meyer Tool and Manufacturing, IL.
 - Advanced Energy Systems, NY.
 - Adron EDM, WI.
 - Ti Fab, PA.
 - Numerical Precision, IL.
 - M-1 Tool Works, IL.

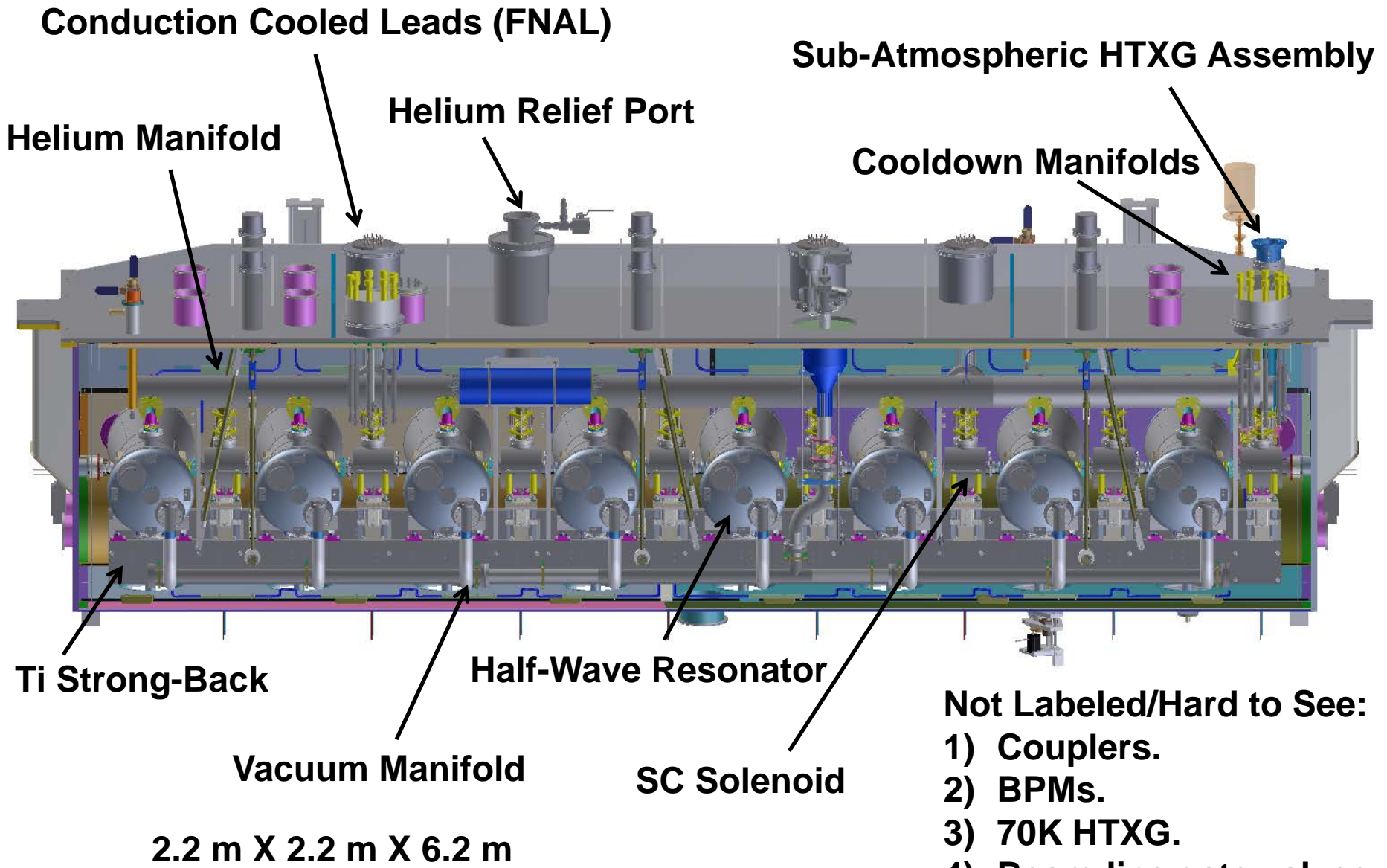


Introduction

- **Building a cryogenic system for the acceleration of H⁻ ions from 2.1 to 10 MeV for PIP-II @ FNAL.**
 - Will contain accelerator cavities and magnets operating at 2 K.
- **Will be the first operational 2 K cryomodule for superconducting accelerator cavities with low-beta ($\beta = v/c < 0.5$) structures.**
 - Using many techniques developed by velocity-of-light (or close to) accelerators; e.g., elliptical cell cavities.
 - Others are in development too; e.g., IFMIF, MSU-FRIB.
- **Design goals for the:**
 - Operate at 2 K instead of 4 K.
 - Further reduce static cryogenic loads relative to previous low-velocity cavity cryomodules.
 - Comply with DOE, ANL and FNAL safety guidelines for cryogenic, vacuum and pressure vessels.
 - Enable faster more-accurate alignment.



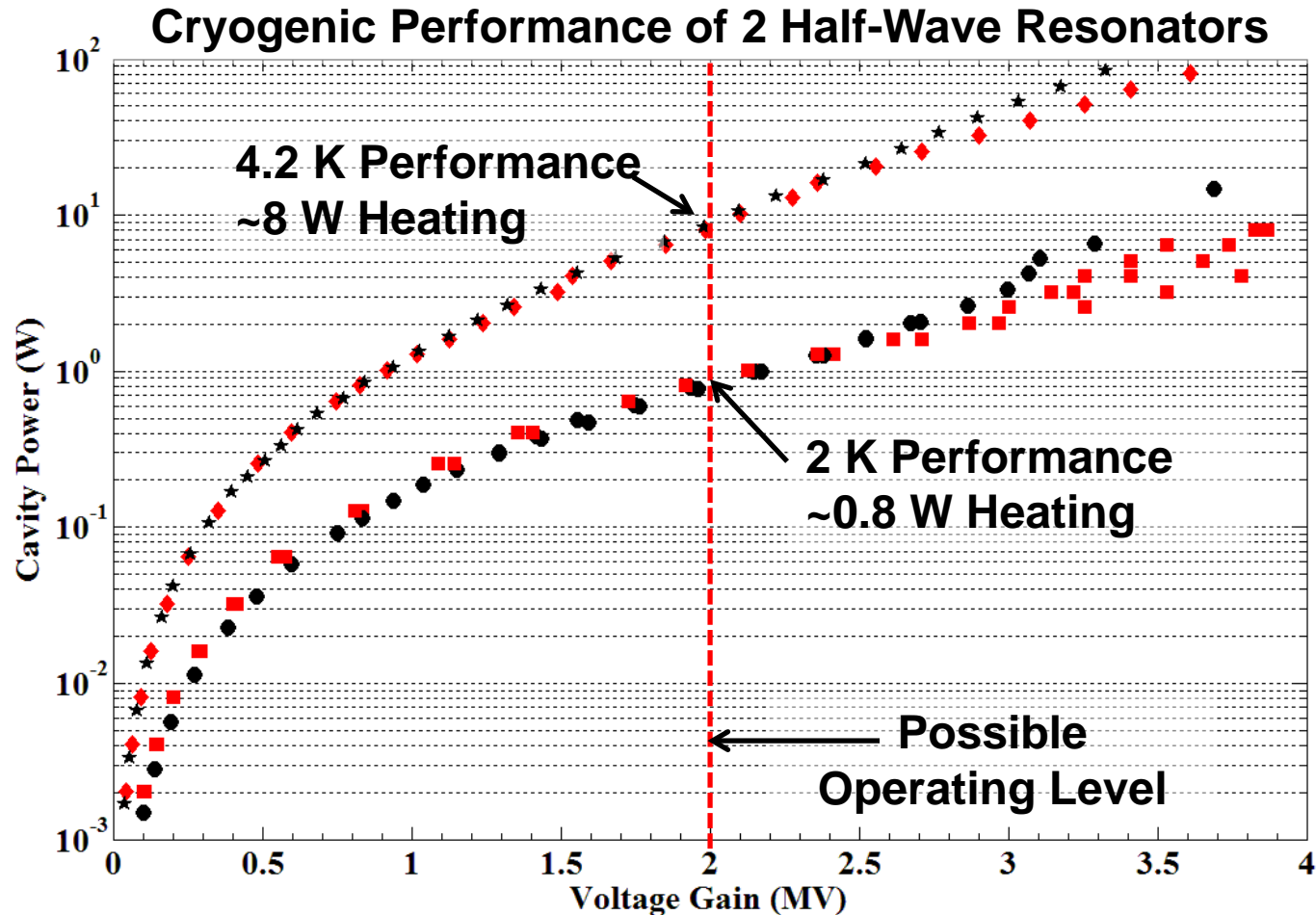
Half-Wave Resonator Cryomodule



- Not Labeled/Hard to See:**
- 1) Couplers.
 - 2) BPMs.
 - 3) 70K HTXG.
 - 4) Beam-line gate valves.

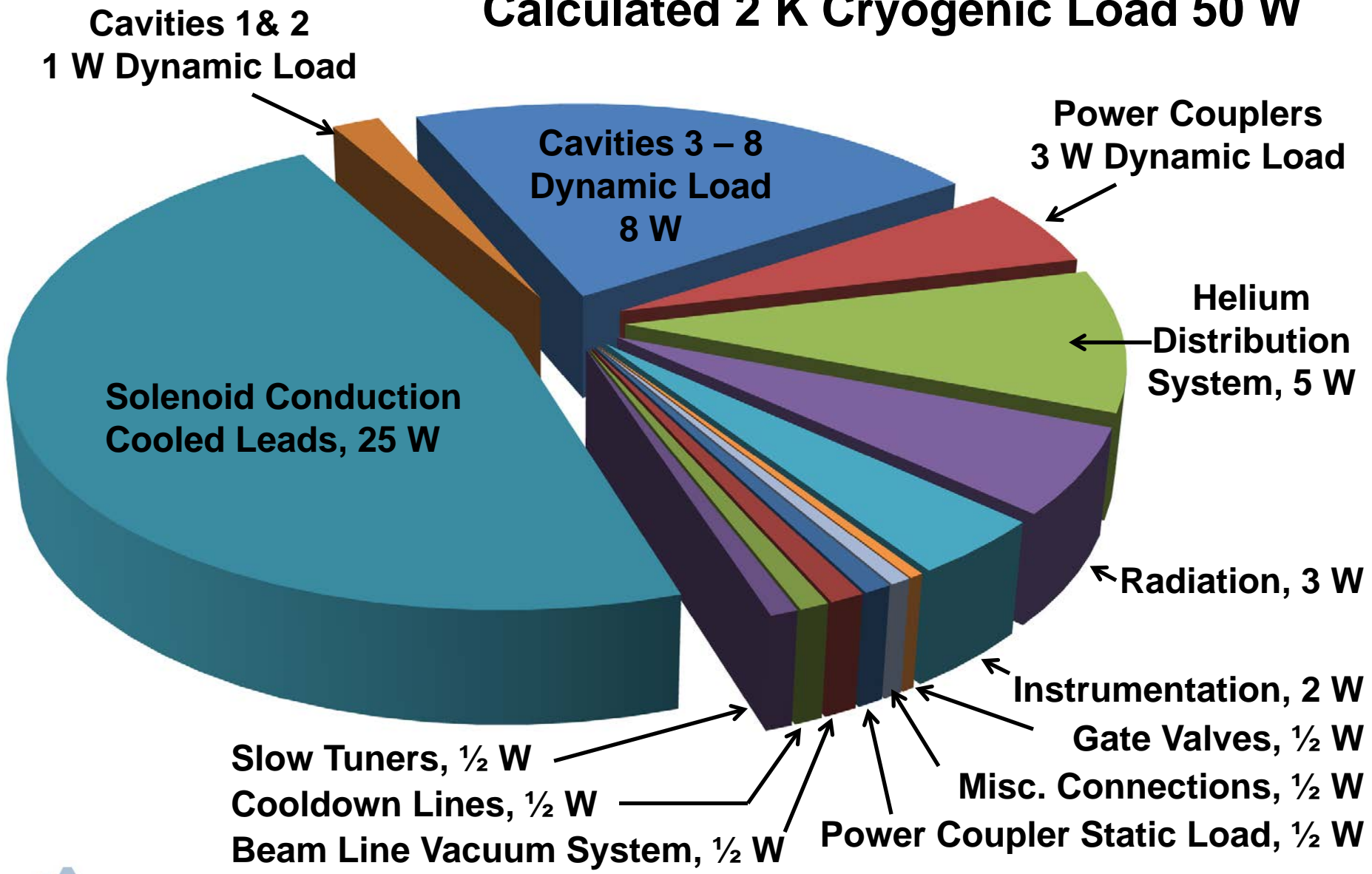
2 K Low-Beta Cavity Cryomodules

- Low-beta = low-frequency and losses scale as f^2 . Low-beta cavities have traditionally operated at 4.2 K to save on refrigeration.
- Why operate at 2 K now?
 - The rest of the system is 2 K = Simplified Cryogenic Distribution.
 - The performance improvement justifies the extra cryogenic cost.



Cryomodule 2 K Design Thermal Loads

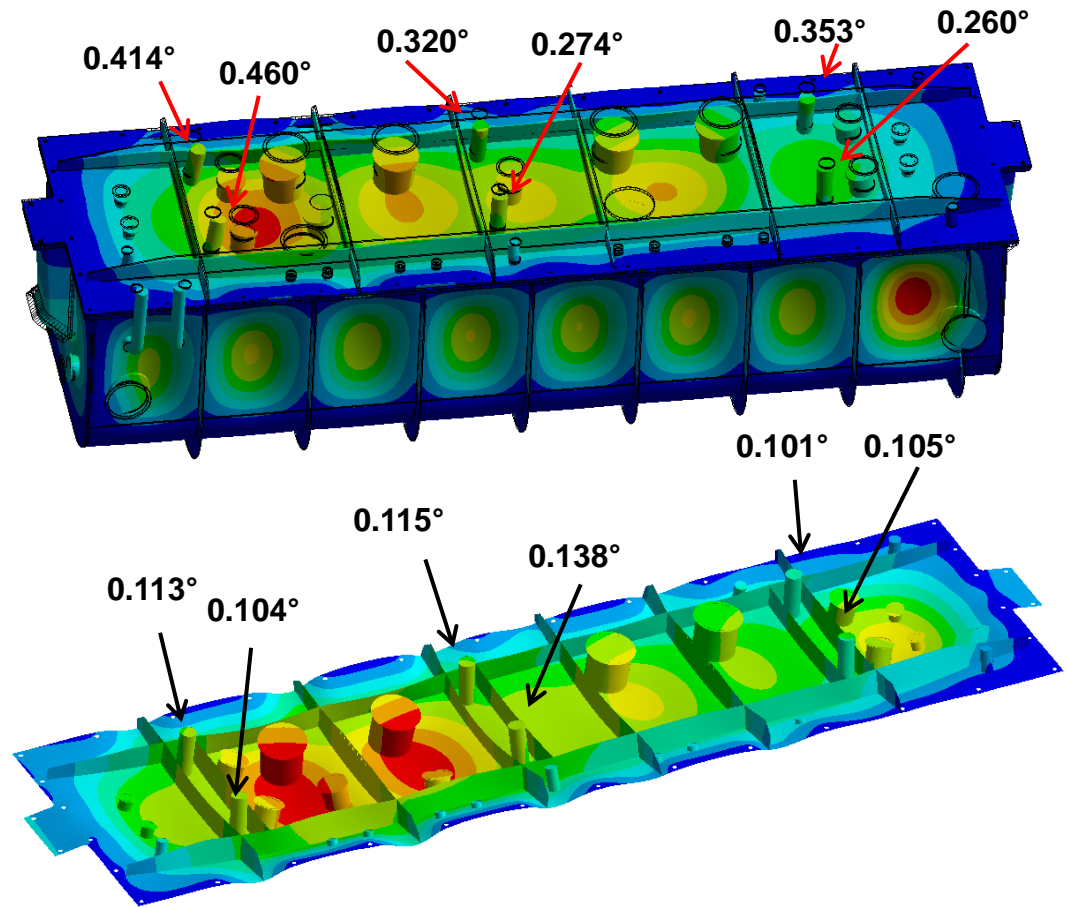
Calculated 2 K Cryogenic Load 50 W



Design: Cavities and Cryomodules

- Design must protect against:
 - Plastic Collapse.
 - Local Failure.
 - Buckling.
 - Failure with Cyclic Loading.
- Design must also:
 - Maintain alignment.
 - Not break penetrations.
- Not discussing solenoids. They receive an ASME U-stamp.

Port Deflection Initial and Final



20°C Material Properties

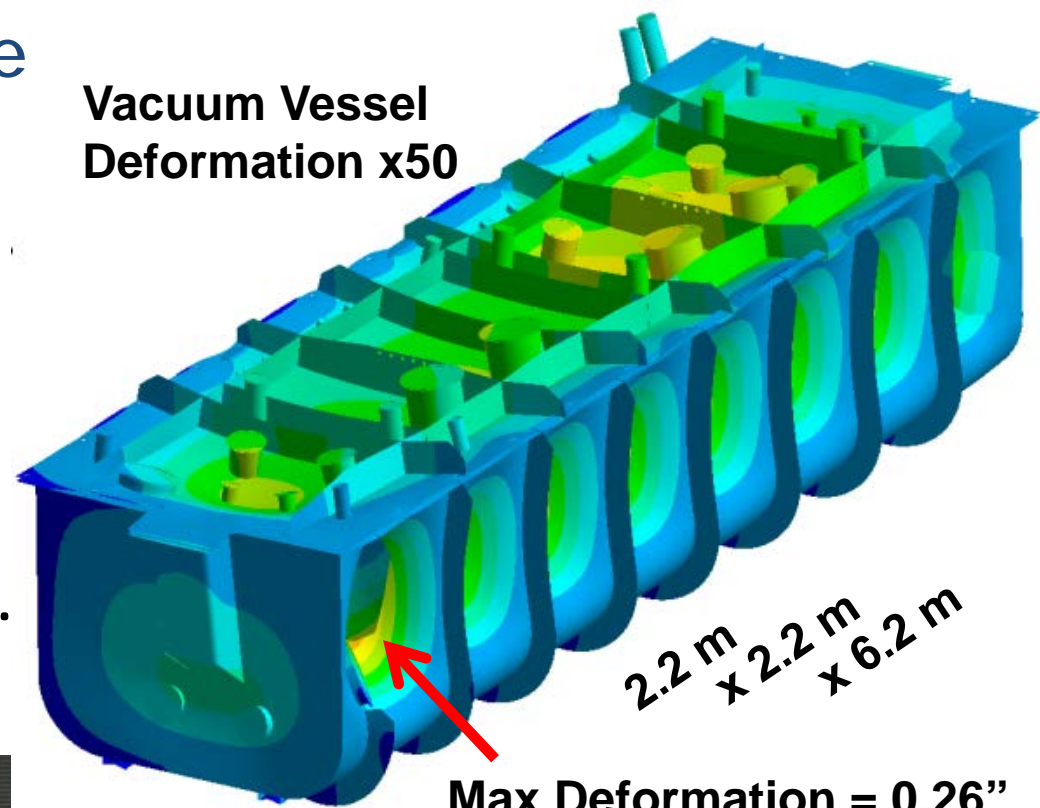
Material	Young's Modulus (ksi)	Poisson's Ratio	Density (lbs/in ³)	Maximum Allowable Stress (ksi)
304 Stainless Steel	29,000	0.270	0.286	20.0
Niobium	15,200	0.396	0.310	5.5



Vessel Design: Cryomodule

- Vacuum Vessel @ 14.7 psiv.
- Used ASME BPVC code to demonstrate protect against:
 - Plastic Collapse (Limit-Load).
 - Local Failure.
 - Buckling.
 - Ratcheting and Cyclic Loading.
- Very safe vacuum vessel.

Vacuum Vessel
Deformation x50



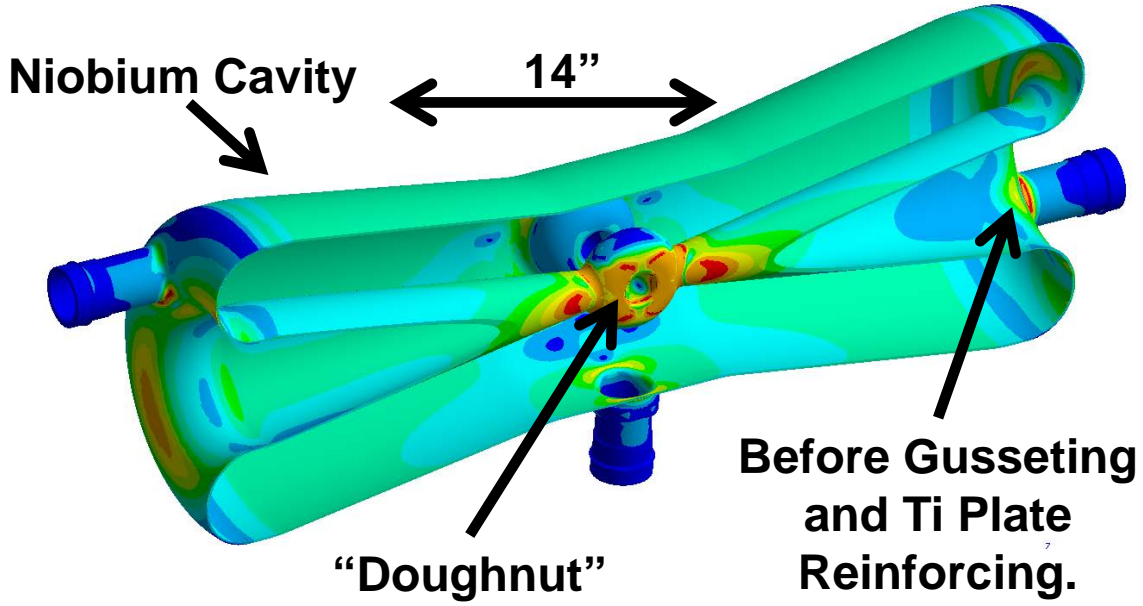
Max Deformation = 0.26"

- Magnetic shielding lines the inner surface of the vacuum vessel.
- 70 K thermal shield inboard of magnetic shield.
 - 32 layers MLI outside.
 - 16 layers MLI inside.



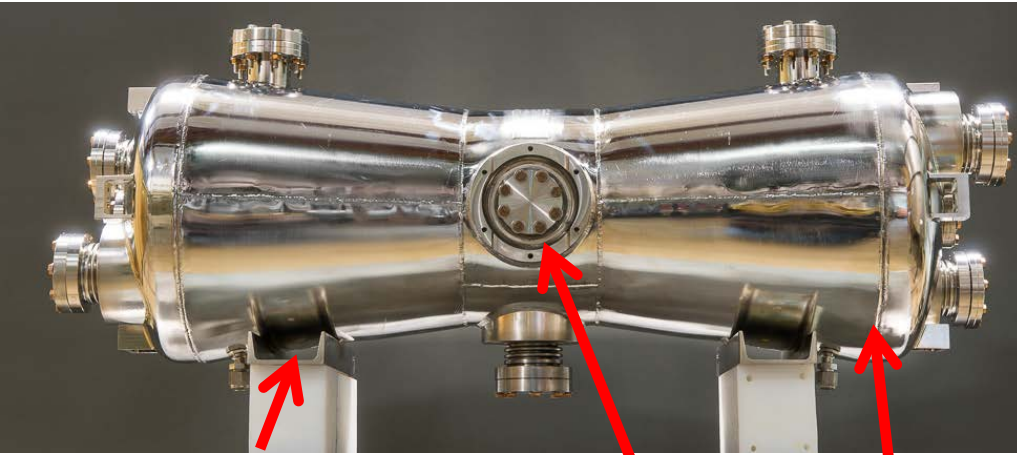
Vessel Design: Cavities

- Design Loads:
 - 2 bar @ R.T.
 - 4 bar @ 2 K.
- Used the rules in the ASME BPVC. No code stamp.
- Used material properties for Nb in compliance with FNAL safety guidelines.



Finished Cavity

Bare Niobium Cavity



Alignment Bracket

Beam Port

Stainless Steel Jacket

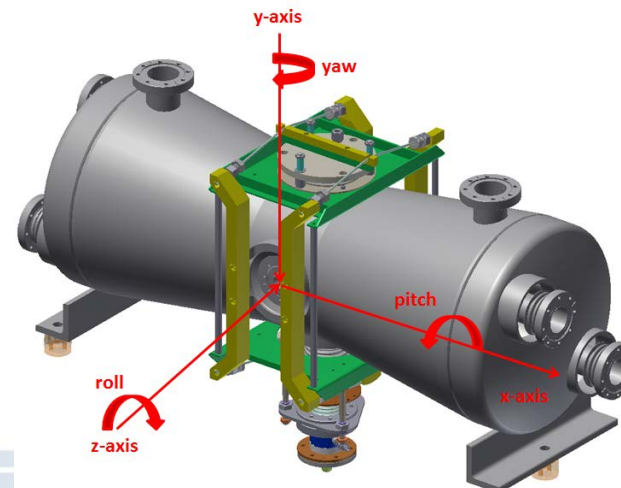
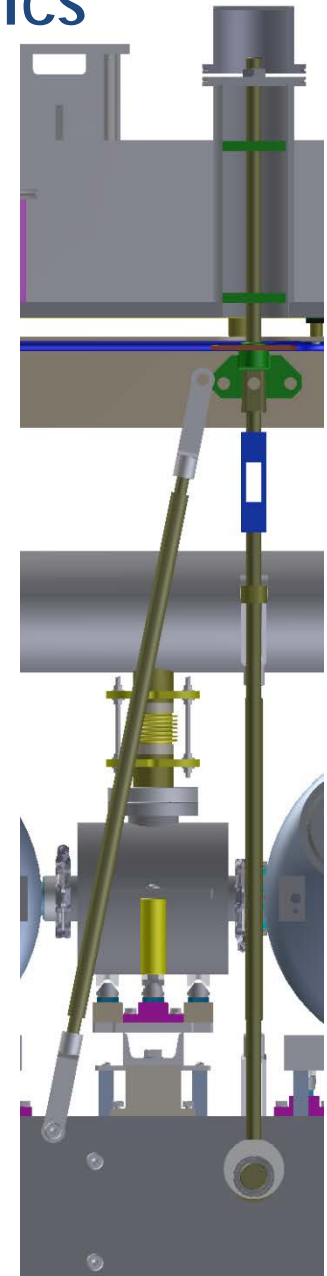
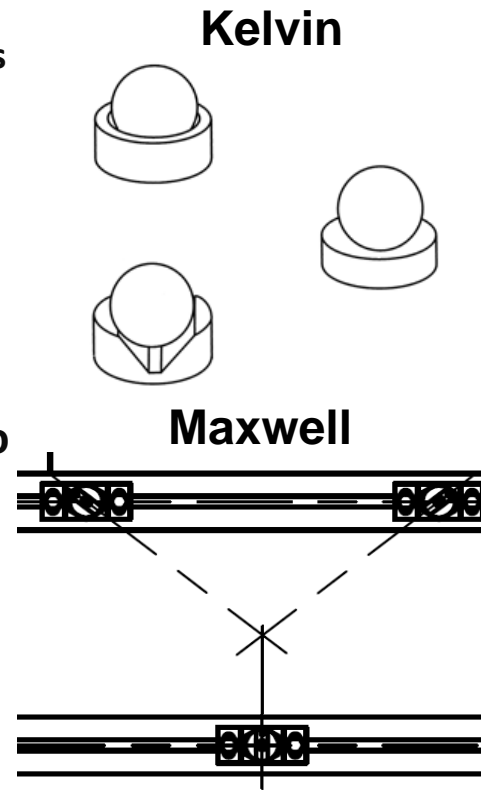
Ti Plate

Power Coupler Port



Alignment - 1: Thermal Contraction & Kinematics

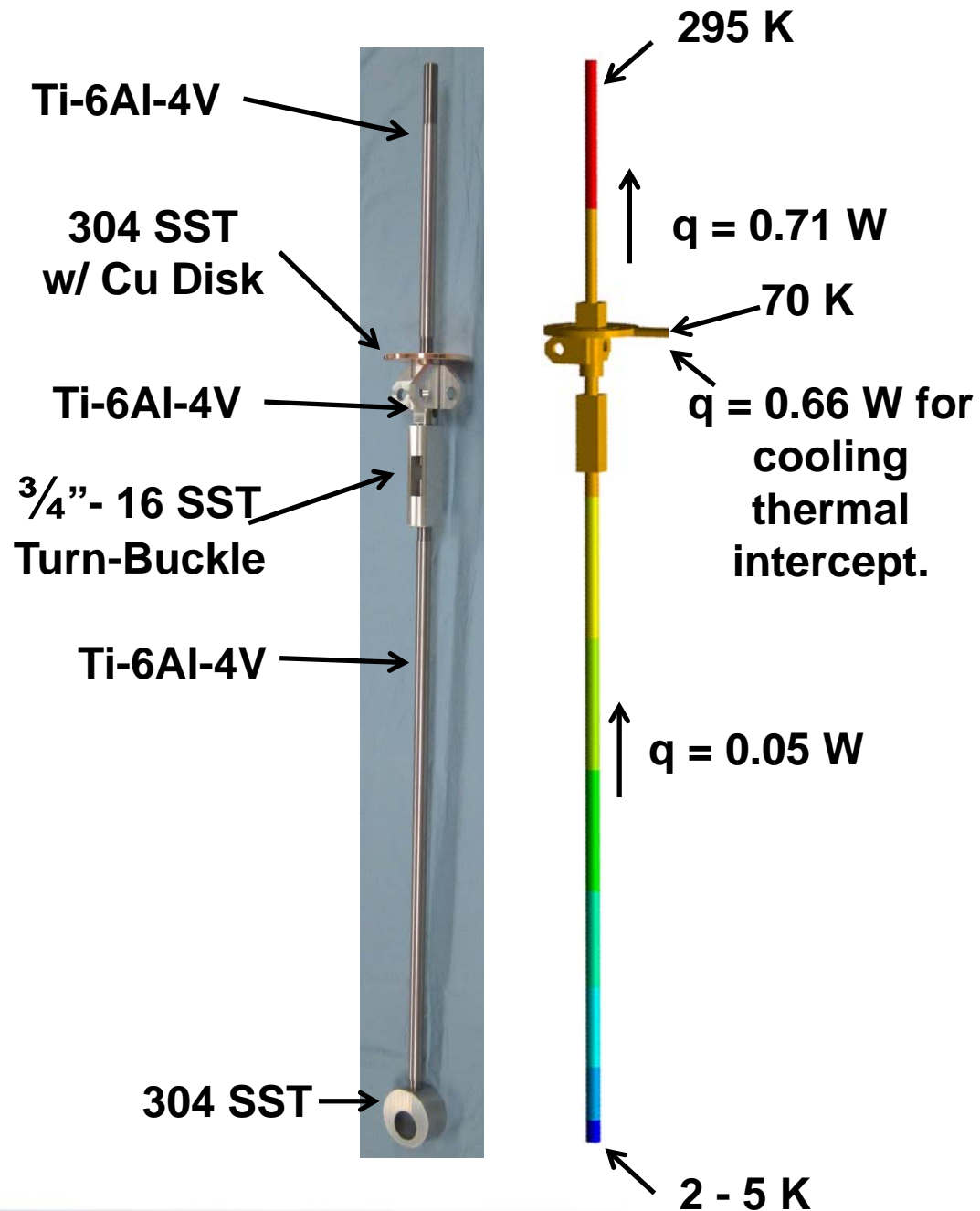
- Need to align solenoids to $\pm 250 \mu\text{m}_{\text{rms}}$ and $\pm 0.1^\circ$ in pitch, yaw and roll relative to the beam axis.
- Transverse shift \sim negligible.
 - We have changed from a Kelvin to a Maxwell planar kinematic coupling.
 - Maxwell geometry can be designed to be thermally invariant.
 - Kelvin geometry shifts toward fixed point.
- Vertical Shift = $650 \mu\text{m}$ up.
 - Hanger Contraction = $+ 1,640 \mu\text{m}$ up.
 - Alignment System contraction = $-990 \mu\text{m}$ up.
 - Possible to zero.



“Design of three-groove kinematic couplings,” A.H. Slocum, Precision Engineering **14**, Pg. 67 (1992).
“Optimal design techniques for kinematic couplings,” Precision Engineering **25**, Pg. 114 (2001).

Cold-Mass Hangers

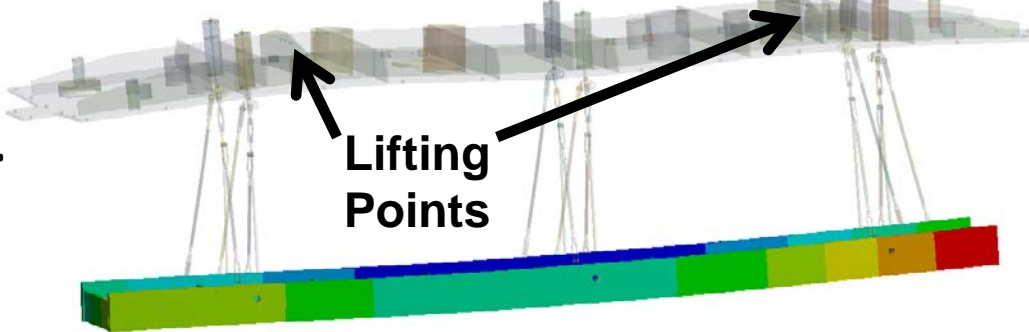
- Hangers have to:
 - Support the 4 ton cold-mass.
 - Allow for adjustment and alignment of the cold-mass.
 - Thermally isolate the ~ 2 K cold-mass from room temperature.
- We take advantage of:
 - Low thermal conductivity materials.
 - Relatively high thermal contact resistance for grease- and lubrication-free connections.



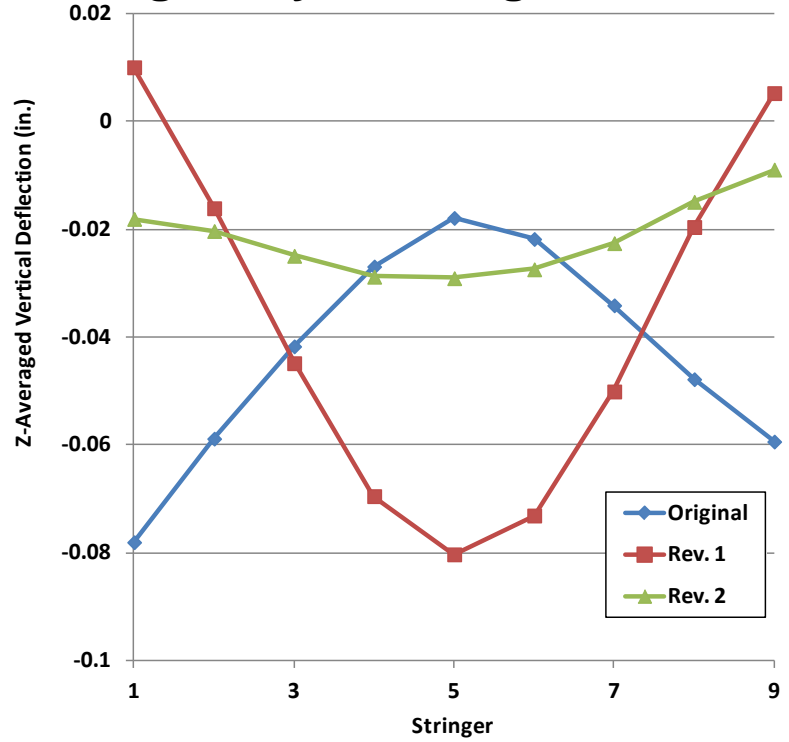
Alignment - 2: Ti Strong-Back

- When lid is on the box the loaded strong-back rails are flat and parallel within 0.005".
- Lifting may perturb the alignment.
- Reduced lifting disturbance via design.

Model of Lid/Strong-Back being Lifted



Lifting Analysis Design Evolution



Strong-Back



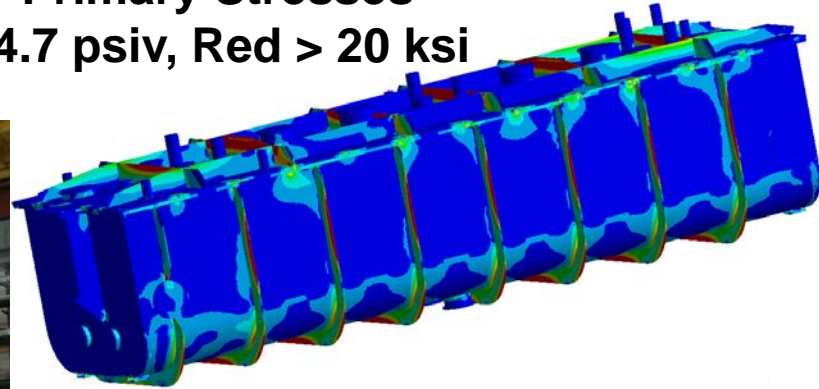
Summary

- At ANL we are developing a 2K superconducting accelerator cavity cryomodule.
- Cryomodule assembly is starting now.
- Hope to test the system without cavities or solenoids late this year.

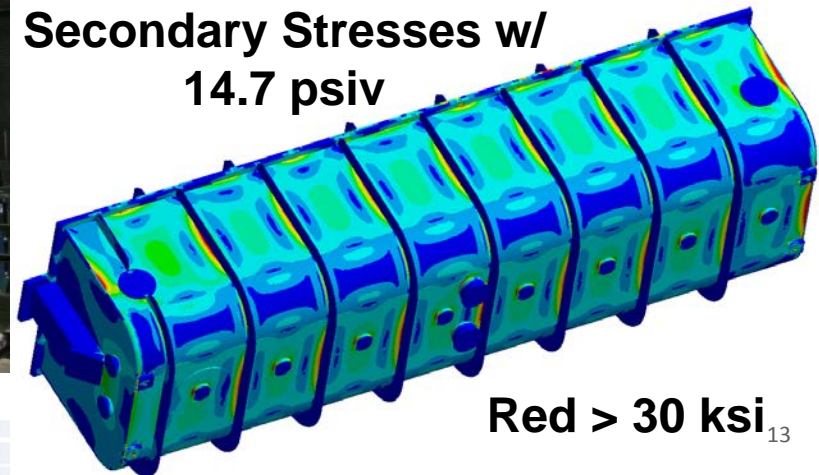
Delivery of Cryomodule @ ANL



Primary Stresses
14.7 psiv, Red > 20 ksi



Secondary Stresses w/
14.7 psiv



Red > 30 ksi

